

The image is a presentation slide for a project titled "Temple Steeple Seismic Design". The background is a photograph of a temple building with a prominent steeple topped by a golden statue. The sky is blue with light clouds. The title is written in large, bold, white sans-serif font on the right side of the slide. Below the title, the text "CHART Engineering . April 2012" is written in a smaller white font. The temple building is light-colored with arched windows and doorways. The text "SANTIDAD AL SEÑOR - LA CASA DEL SEÑOR" is visible on the facade of the building.

# Temple Steeple Seismic Design

CHART Engineering . April 2012

SANTIDAD AL SEÑOR - LA CASA DEL SEÑOR



# 1 THE CHALLENGE

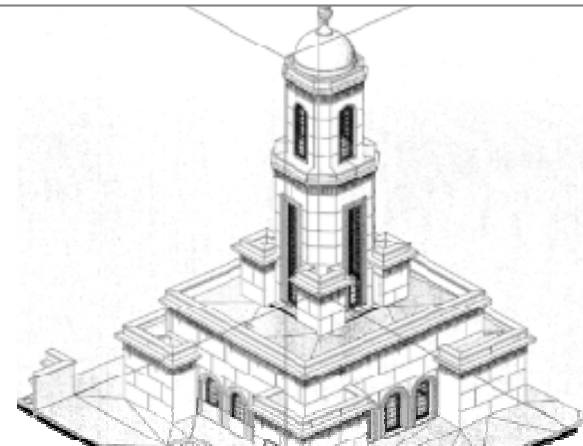
Design a temple steeple located in a high seismic area while optimizing cost and keeping to architectural constraints.

## ARCHITECTURAL CONSTRAINTS

- No steel framing crossing large windows
- One beam of light from bottom to top
- Octagonal steeple shape
- Angel Moroni
- Heavy Cladding

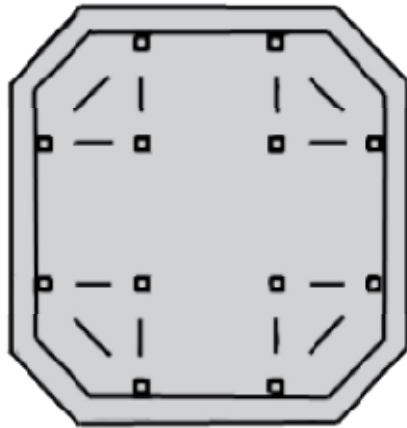
## SEISMIC CONSTRAINTS

- High seismic activity area
- Seismic category E
- Minimized deflection
- Safe for Maximum Considered Earthquake

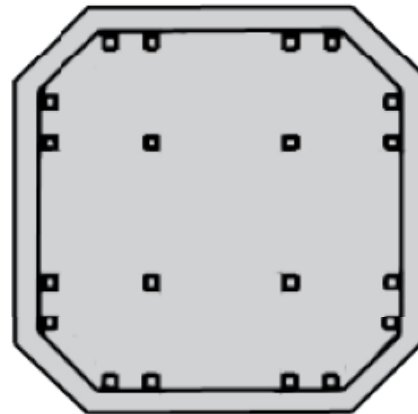




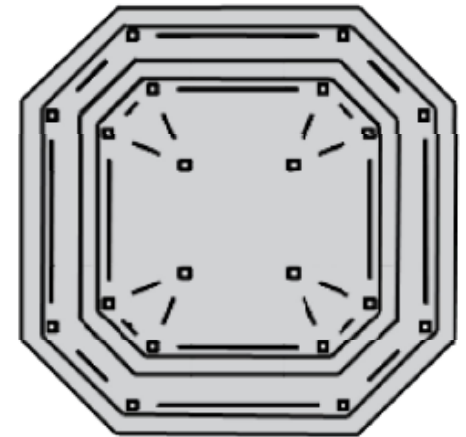
# 2 THE PROCESS



Ineffective design because of gap between members and cladding.



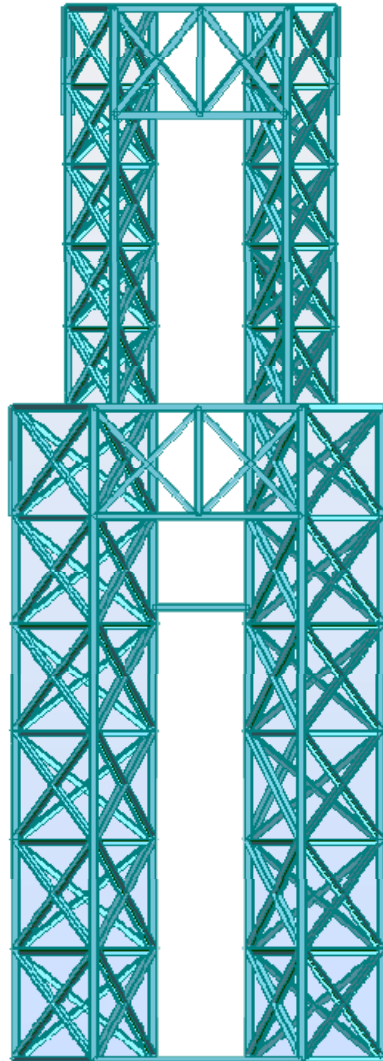
Ineffective use of steel: not cost efficient.



Allows cladding to be attached at top while reducing steel members.



The steeple was designed as a special concentrically braced frame, using the two-stage analysis approach from ASCE 7-10.



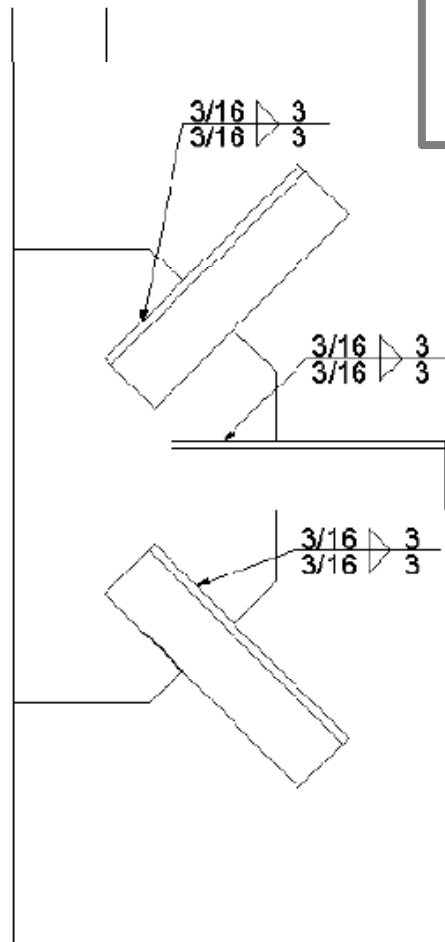
The two-stage approach required certain conditions to be met. This approach was desirable because it resulted in a lower seismic force.

- Period of base structure cannot be 1.1 times more than period of top structure
- Base structure and steeple must have separate R and p values
- The ratio of R/p of the base to R/p of the steeple must be less than 1

<b>Period Requirement</b>	$T_{base}$	0.18
	$T_{steeple}$	0.13
	$1.1 * T_{steeple}$	0.143
<b>R and P Requirement</b>	$R_{steeple}$	6
	$P_{steeple}$	1.3
<b>R and P Ratio Requirement</b>	$R/p_{base}$	0.85
	$R/p_{steeple}$	4.62
	Ratio	0.83



Connections for special concentrically braced frames are very difficult to design and require many AISC standards to be met.



**As simplification reduces cost, three-inch welds were found to be sufficient for the largest loads and were thus used for all connections.**



$$E_m = E_{mh} + E_v$$

Seismic force is computed by the sum of horizontal and vertical components.

$$E_{mh} = \Omega_o * Q_E$$

$$E_v = 0.2 * S_{DS} * D$$

Other variables rely on parameters such as soil properties, height of tower, and other seismic constraints.

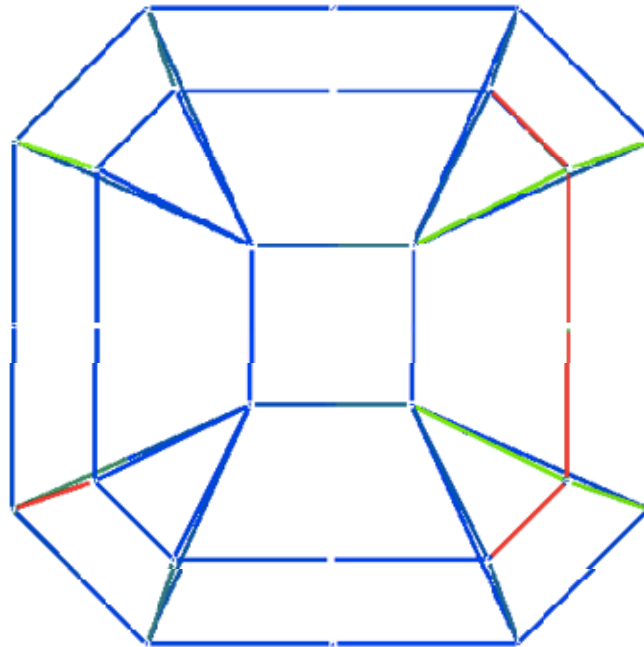
After calculations , the seismic force was computed as 34.9 kips.



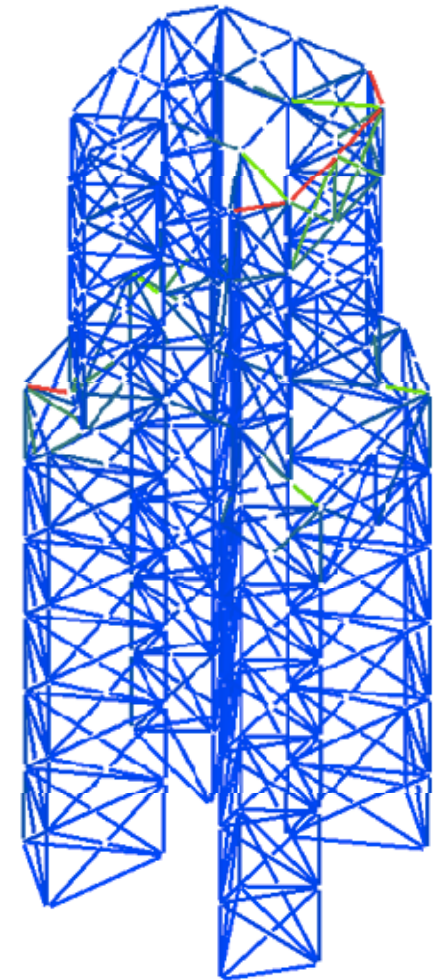


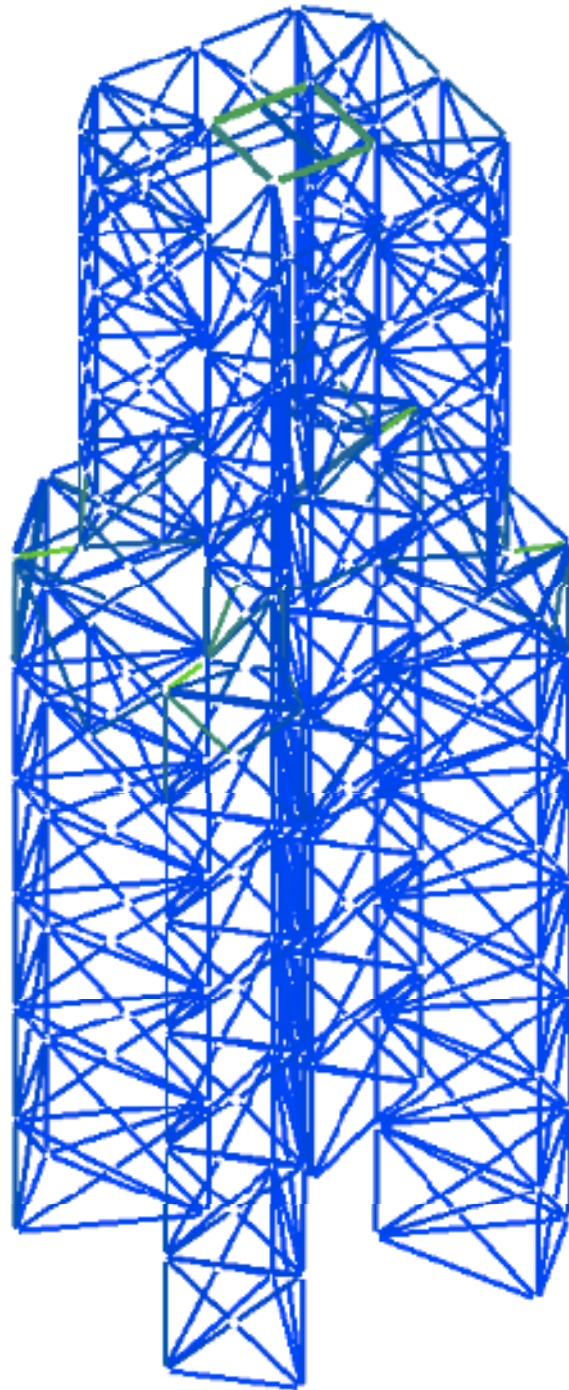
# 3 THE ANALYSIS

Visual Analysis was used to test the design under loading:  
Both from dead weight and seismic loading.

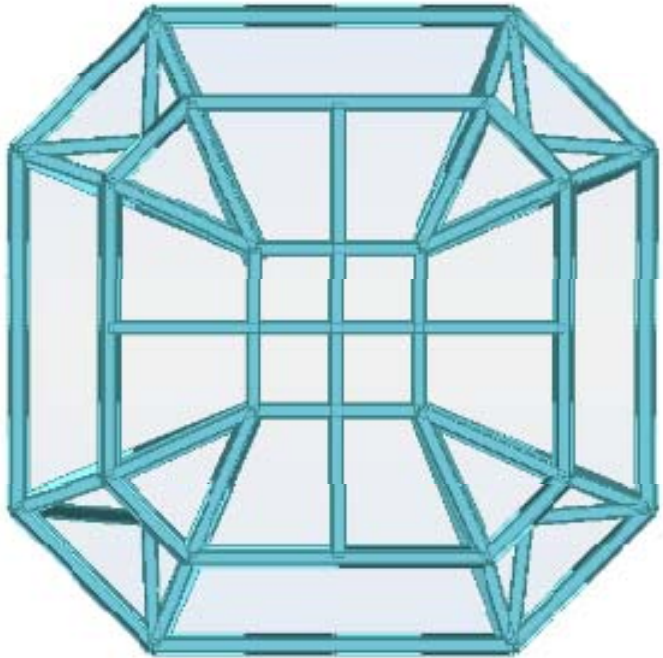


Our prepared design had failure in two main locations, the top of the tower and where the two levels meet.





Adding just a few more members gave a sturdy design, while allowing all local steel to remain.

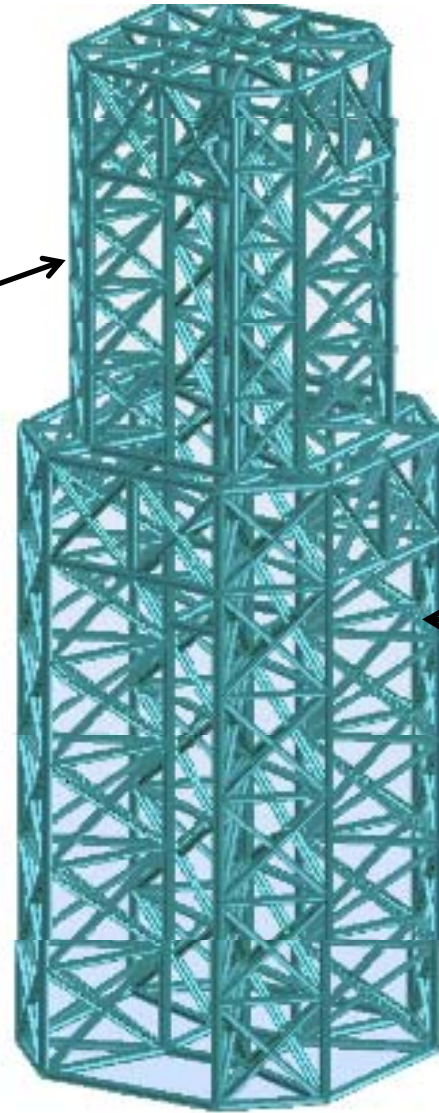






# 4 THE SOLUTION

HSS4x4x5/16 were used as the columns and bracing at critical locations.



2L3x3x3/16 were used for all cross bracing.

# Cost Analysis

Optimizing cost was a large part of the overall consideration for design. There are a few main ways to reduce cost in a design. They are:

- Reduce steel used
- Use local materials
- Type of connections
- Simplify design

Labor costs are the most significant in any steel project. We reduced these costs by

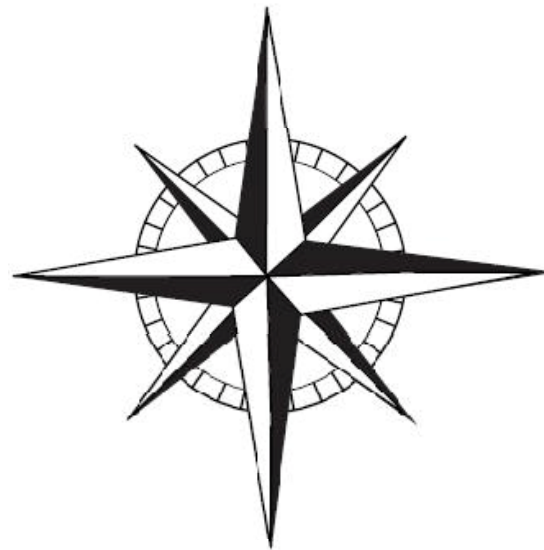
- Only using two steel member sizes
- Using welded connections out of the country do not cost significantly more than bolted connections
- We also used 100% local steel, reducing steel ordering costs significantly





# 5 THE FUTURE

The design could be improved upon by continuing to analyze the steel structure to see which steel members are unnecessary. This could further reduce cost.



# CHART